

# Electro-Osmosis With Corrected Solution of Poisson-Boltzmann Equation That Satisfies Charge Conservation Principle

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(Dated: September 13, 2014)

## Abstract

We derive the electro-osmotic velocity profile in a micro-channel using a recently corrected charge density distribution within an electrolytic solution. Previous distribution did not take care of charge conservation principle while solving Poisson-Boltzmann equation and needed modification, hence the velocity profile also needs modification that we do here. Helmholtz-Smoluchowskii velocity scale is redefined, which accommodates Debye length parameter in it, unlike old definition.

**PACS numbers:** 47.61.-k, 82.45.-h, 47.65.-d, 85.85.+j

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Electro-osmosis concerns driving an electrolytic solution through a narrow channel using an externally applied axial electric field, exploiting a possible non-trivial charge density distribution ( $\rho_e$ ) in the solution. It has a very old history [1, 2] and finds applications in many fields [3–5]. Now,  $\rho_e$  appears in the body force term in the fluid momentum equation, which takes a very simple form for a flow with small Reynolds number (typical for a narrow channel) and when the flow is steady and hydrodynamically fully developed. For a rectangular geometry, the momentum equation is given by [6, 7]:

$$0 = \mu \frac{d^2 v}{dx^2} + E_y \rho_e \quad (1)$$

$\rho_e$  and fluid velocity  $v$  vary essentially along the smallest side ( $2a$ ) of geometry ( $x$  direction);  $E_y$  is external electric field, applied in  $y$  direction;  $\mu$  is uniform viscosity. Now, solving Poisson-Boltzmann (PB) equation we obtain  $\rho_e$  as spatial function that is needed to solve the above equation. However, the old solution [8, 9] did not take care of charge conservation principle properly. This author attempted to remove that discrepancy in Ref [10, 11], and obtained a velocity profile using it in Ref [7]. However, that formulation for  $\rho_e$  still had problem, for it was not satisfying Poisson's equation in general. Finally, the correct expression for  $\rho_e$  (scaled) has been developed in Ref [12], and is given by,

$$\rho_e^* = \frac{1}{2 \sinh(\kappa)} [q_0 \kappa \cosh(\kappa \eta) - \delta \sinh(\kappa \eta)] \quad (2)$$

Meaning of symbols can be found in Ref [7, 12]. We mention them briefly:

$$\kappa \equiv a/\lambda_D; \quad \eta \equiv x/a; \quad \rho_e^* \equiv \rho_e/\rho_0; \quad \rho_0 \equiv (\epsilon \kappa^2 \zeta/a^2) \quad (3)$$

Where,  $\lambda_D$  is Debye length [8];  $\epsilon$  is permittivity of liquid;  $\zeta$  is a suitable scale for electrostatic potential  $\psi$ , ( $\zeta > 0$ ).

$\delta$  is the potential difference between walls at  $\eta = +1$  and  $\eta = -1$ . If  $Q_0$  is the net charge present in liquid ( in a cross-section, per unit axial length),  $\int_{-1}^{+1} \rho_e^* d\eta = Q_0/\rho_0 \equiv q_0$ , ( using Eq. 3). Now, using Eq. 3 and Eq. 2, we can write Eq. 1 as,

$$\begin{aligned} \frac{d^2 v}{d\eta^2} &= - \left( \frac{a^2 E_y \rho_0}{\mu} \right) \rho_e^* \\ &= - \left( \frac{\epsilon \zeta E_y}{\mu} \right) \kappa^2 \rho_e^* \\ &= -M \kappa^2 [q_0 \kappa \cosh(\kappa \eta) - \delta \sinh(\kappa \eta)] \end{aligned} \quad (4)$$

$$\text{Where, } M \equiv \left( \frac{\epsilon \zeta E_y}{2\mu \sinh(\kappa)} \right) \quad (5)$$

Intergrating Eq. 4 twice w.r.t  $\eta$  we get,

$$v = -M [q_0\kappa \cosh(\kappa\eta) - \delta \sinh(\kappa\eta)] + C_1\eta + C_2 \quad (6)$$

We use no-slip conditions at both walls, i.e.  $v = 0$  at  $\eta = \pm 1$ . Hence,

$$0 = -M [q_0\kappa \cosh(\kappa) - \delta \sinh(\kappa)] + C_1 + C_2 \quad (7)$$

$$0 = -M [q_0\kappa \cosh(\kappa) + \delta \sinh(\kappa)] - C_1 + C_2 \quad (8)$$

From Eq. 7 and Eq. 8 we solve for  $C_1$  and  $C_2$  and get,

$$C_1 = -M\delta \sinh(\kappa) \quad (9)$$

$$C_2 = Mq_0\kappa \cosh(\kappa) \quad (10)$$

Using Eq. 9 and Eq. 10 in Eq. 6 and rearranging terms,

$$\begin{aligned} v &= M [q_0\kappa (\cosh(\kappa) - \cosh(\kappa\eta)) - \delta (\eta \sinh(\kappa) - \sinh(\kappa\eta))] \\ &= M \left[ q_0\kappa \cosh(\kappa) \left( 1 - \frac{\cosh(\kappa\eta)}{\cosh(\kappa)} \right) - \delta \sinh(\kappa) \left( \eta - \frac{\sinh(\kappa\eta)}{\sinh(\kappa)} \right) \right] \\ &= M\kappa \cosh(\kappa) \left[ q_0 \left( 1 - \frac{\cosh(\kappa\eta)}{\cosh(\kappa)} \right) - \delta \frac{\tanh(\kappa)}{\kappa} \left( \eta - \frac{\sinh(\kappa\eta)}{\sinh(\kappa)} \right) \right] \end{aligned} \quad (11)$$

Now, using Eq. 5 we get,

$$\begin{aligned} M\kappa \cosh(\kappa) &= \frac{\epsilon\zeta E_y}{2\mu \sinh(\kappa)} \kappa \cosh(\kappa) \\ &= \lambda_{||} \frac{\epsilon\zeta E_0\kappa}{2\mu \tanh(\kappa)} \end{aligned} \quad (12)$$

$$\text{Where, } \lambda_{||} \equiv \frac{E_y}{E_0}, \text{ with } E_0 > 0$$

Let us define corrected Helmholtz-Smoluchowskii velocity scale  $v_{H.S.Corr}$  by,

$$v_{H.S.Corr} \equiv \frac{\epsilon\zeta E_0\kappa}{2\mu \tanh(\kappa)} \quad (13)$$

It differs from old Helmholtz-Smoluchowskii velocity scale, see Ref [8]. Let  $\bar{v} \equiv v/v_{H.S.Corr}$ .

Finally we arrive at,

$$\bar{v} = \lambda_{||} \left[ q_0 \left( 1 - \frac{\cosh(\kappa\eta)}{\cosh(\kappa)} \right) - \delta \frac{\tanh(\kappa)}{\kappa} \left( \eta - \frac{\sinh(\kappa\eta)}{\sinh(\kappa)} \right) \right] \quad (14)$$

When we reverse  $E_y$ , velocity field must reverse too. In the above equation, the sign of  $\lambda_{||}$  changes when we reverse  $E_y$ , and hence  $\bar{v}$  changes sign as expected; in old works it was not

possible to capture this reversal of direction in the scaled velocity, because  $v_{H,S}$  was not defined properly. This author made an attempt to correct it in Ref [7], however  $\rho_e$  was still not correct there. We can control the fluid flow easily using the potential difference.

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