# The Emergence Mechanism and Calculation Method of Turbulent Flows

### Abstract

An explanation is offered of the mechanism of turbulent flows emergence, based of the Maxwell-like gravitation equations, updated after some known experiments. It is shown that the moving molecules of flowing liquid interact like electrical charges.

The forces of such interaction can be calculated and included to the Navier-Stokes equations as mass forces. Navier-Stocks equations complemented by these forces become equations hydrodynamics for turbulent flow. For the calculations of turbulent flows the known methods of Navier-Stokes equations solution may be used.

The source of energy in cavitation heat generators is considered.

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### **1. Introduction**

In [1] an analogy of electromagnetism and gravitoelectromagnetism has been explored. From the point of this analogy the new experiments of Samokhvalov [2] have been analyzed. Based on this analysis it was shown there, that Maxwell-like equations of gravitoelectromagnetism should be supplemented by a certain empirical coefficient of gravitational permeability of the medium. For vacuum this

coefficient is about  $\xi \approx 10^{12}$ , and it decreases rapidly with the pressure increase. This explains the absence of visual effects of gravito-magnetic interaction of moving masses in the air. However in vacuum theses interactions are clearly visible in the above mentioned experiments.

In the liquid flow the moving molecules are separated by vacuum. So their gravito-magnetic interaction forces can be substantial and influence the nature of the flow.

We know that with increasing speed of laminar liquid or gas turbulence may occur spontaneously ( without the influence of external forces) [3]. The mechanism for turning from laminar to turbulent flow has not been found. Evidently, a source of forces perpendicular to the flow speed must be found.

Further it is shown that the gravito-magnetic interaction of the moving liquid masses can be the cause of the turbulence emergence.

## **2. The Interaction of Moving Electrical Charges**

Let us consider two charges  $q_1$  and  $q_2$ , moving with speeds  $v_1$ and  $v_2$  accordingly. It is known [4], that the induction of the field created by the charge  $q_1$  in the point in which the charge  $q_2$  is located, is equal (here and further we are using the СGS System)

$$
\overline{B_1} = q_1 \left( \overline{v_1} \times \overline{r} \right) / c r^3 \,. \tag{1}
$$

Here the vector  $r$  is directed from the point where the moving charge  $q_1$  is located. The Lorentz force acting on the charge  $q_2$ , is

$$
\overline{F_{12}} = q_2 \left( \overline{v_2} \times \overline{B_1} \right) / c \,. \tag{2}
$$

Similarly,

$$
\overline{B_2} = q_2 \left(\overline{v_2} \times \overline{r}\right) / c r^3, \tag{3}
$$

$$
\overline{F_{21}} = q_1 \left( \overline{v_1} \times \overline{B_2} \right) / c \,. \tag{4}
$$

In the general case  $F_{12} \neq F_{21}$  , i.e. the third Newton law does not work  $-$  there are unbalanced forces acting on the charges  $q_1$  and  $q_2$  and bending the trajectories of these charges movement.

Let us consider the correlation between the Lorentz force and the force of charges attraction. In the simplest case the Lorentz force found from  $(1, 2)$  is

$$
F = \frac{q_1 q_2 v_1 v_2}{r^2 c^2}.
$$
\n<sup>(5)</sup>

The force of attraction of the two charges is

$$
P = \frac{q_1 q_2}{r^2}.
$$
\n<sup>(6)</sup>

Consequently,

$$
\phi_e = \frac{F}{P} = \frac{v_1 v_2}{c^2}.
$$
\n<sup>(7)</sup>

We shall call this magnitude the efficiency of Lorentz forces.

### **3. Gravito-Magnetic Interaction of Moving Masses**

In analogy with the electrical charges interaction, two masses *<sup>m</sup>*1 and  $m_2$ , moving with speeds  $v_1$  and  $v_2$  accordingly are also interacting. In [1] it is shown that in this case there emerge gravitomagnetic inductions of the form:

$$
\overline{B_{g1}} = Gm_1(\overline{v_1} \times \overline{r})/cr^3, \qquad (1)
$$

$$
\overline{B_{g2}} = Gm_2(\overline{v_2} \times \overline{r})/cr^3, \qquad (2)
$$

where

 $c$  — the speed of light in vacuum,  $c \approx 3\!\cdot\! 10^{10}$  [cm/sec];

 $G$  - gravitational constant,  $G \approx 7 \cdot 10^{-8}$  [dynes·cm<sup>2</sup>·g<sup>-2</sup>]. The masses are also affected by the Lorentz gravito-magnetic Lorentz

forces of the following form [1]:

$$
\overline{F_{12}} = \varsigma \xi \, m_2 \left( \overline{v_2} \times \overline{B_{g1}} \right) / c \,, \tag{3}
$$

$$
\overline{F_{21}} = \varsigma \xi m_1 \left(\overline{v_1} \times \overline{B_{g2}}\right) / c \,, \tag{4}
$$

where

 $\zeta = 2$ , which follows from GRT,

 $\xi \approx 10^{12}$  - the gravitational permeability coefficient for vacuum [1].

For parallel speeds and equal mass forces  $F_{12} = -F_{21}$  the laminar flow keeps its character. However, in the general case, when  $v_1 \neq v_2$ , the forces  $F_{12} \neq F_{21}$  are generated, i.e. the unbalanced force

 $\Delta F = F_{12} + F_{21}$ , acting on the masses  $m_1$  and  $m_2$  and bending the trajectories of these masses movement (let us note that here the Newton's third law is not observed [4]). From the above formulas follows that the unbalanced force is directed at an angle to the flow speed, which violates the laminarity.

Let us find the correlation between the Lorentz gravito-magnetic force and the masses attraction force. Similarly to the previous, in the simplest case Lorentz gravito-magnetic force may be found from  $(1, 3)$ :

$$
F = \zeta \xi \frac{Gm_1m_2v_1v_2}{r^2c^2}.
$$
\n<sup>(5)</sup>

The attraction force of two masses is

$$
P = \frac{Gm_1m_2}{r^2}.
$$
 (6)

Thus,

$$
\phi_g = \frac{F}{P} = \zeta \xi \cdot \frac{v_1 v_2}{c^2}.
$$
\n(7)

We shall call this magnitude – the Lorentz gravito-magnetic force efficiency Comparing (2.7) and (3.7) we find that

$$
\phi_g = \phi_e \varsigma \tilde{\xi} \tag{8}
$$

Consequently, the efficiency of Lorentz gravito-magnetic forces is much higher than Lorentz electromagnetic forces efficiency for comparable speeds.

### **4. Gravito-Magnetic Interaction as the Cause of Turbulence**

For the appearance of unbalanced forces the following conditions must be satisfied:

- 1. the speeds must be of certain magnitude (which make these forces substantial);
- 2. there must be a cause for local change of the speeds, for instance
	- o an appearance of a barrier,
	- o a change of pressure when a stream flows from the water.

There may be a number of reasons increasing the unbalanced forces:

- Temperature rise causing the speeds  $v_1$  and  $v_2$  to cease being parallel due to heat fluctuations,
- Viscosity reduction, i.e. the reduction of intermolecular attraction forces which counteract the unbalanced forces that take the molecules apart.

We may specify also a number of external factors causing the appearance of unbalanced forces due to external violation of speeds  $v_1$  and  $v_2$ parallelism, for instance:

- abrupt changes in temperature, pressure;
- the injection of extra liquid or other agent.

A local change of equal speeds of a pair of linked molecules, caused, for instance, by asymmetric blow, is inevitably spread to the whole flow area.

The Navier-Stokes equations permit to determine of a speed of flow that meets a barrier or leaves a barrier. Knowing these speeds, we may determine unbalanced forces from the said equations. Then these forces as the functions of speeds, may be included into the Navier-Stokes equations as the mass forces.

The kinetic energy of turbulent motion increases with increasing turbulence. This increase occurs due to the action of gravitomagnetic forces of Lorentz. The source of these forces and this additional energy is (as shown above) the gravitational field of the Earth.

There are devices in which this additional energy is used - so-called cavitation heat generators. The first such device was "Apparatus for Heating Fluids" by J. Griggs [8]. There are devices in which this additional energy is used - so-called cavitation heat generators. The first such device was "Apparatus for Heating Fluids" by J. Griggs [8]. In it *"the rotor rides a shaft which is driven by external power means. Fluid injected into the device is subjected to relative motion between the rotor and the device housing, and exits the device at increased pressure and/or temperature"*. At present, there are many such devices that differ in the ways of creating turbulent motion see, for example, [9], where there are also references to many prototypes. Such devices provide efficient, simply, inexpensive and reliable sources of heated water and other fluids for residential and industrial use*.*

Together with the existence of cavitation heat generators there is no generally accepted theory that reveals the source of additional energy that appears as a result of the functioning of these cavitation heat generators. In particular, Griggs in [8] points out that his *"device is*  *thermodynamically highly efficient, despite the structural and mechanical simplicity of the rotor and other compounds"*, but does not provide a theoretical justification for this statement. The authors of the following devices also do not consider the reasons for the efficiency of their devices.

All this confirms that the source of the additional energy of the cavitation heat generators is the gravitational field of the Earth.

### **5. Quantitative Estimates**

In the general case, from (3.2, 3.4) we can find

$$
\overline{F_{21}} = \frac{\varsigma \xi G m_1 m_2}{c^2 r^3} \left( \overline{v_1} \times (\overline{v_2} \times \overline{r}) \right).
$$
 (1)

Let us consider the vectors' orts, denoting them by a stroke. Then from  $(1)$  we get:

$$
\overline{F_{21}} = \sigma \overline{f_{21}} \,, \tag{2}
$$

where

$$
\overline{f_{21}} = (\overline{v_1'} \times (\overline{v_2'} \times \overline{r'})).
$$
\n(3)

$$
\sigma = \frac{\varsigma \xi G \cdot m_1 m_2 v_1 v_2}{c^2 r^2},\tag{4}
$$



Fig. 1.

In the same way,

$$
\overline{F_{12}} = \sigma \overline{f_{12}}\,,\tag{5}
$$

where

$$
\overline{f_{12}} = (\overline{v_2'} \times (\overline{v_1'} \times \overline{r'})), \tag{6}
$$

and

$$
\overline{\Delta F} = \sigma \overline{\Delta f} \,, \tag{7}
$$

where

$$
\overline{\Delta F} = \overline{F_{21}} + \overline{F_{12}},
$$
\n(8)

$$
\Delta f = f_{21} + f_{12}.\tag{9}
$$

Let us consider two adjacent molecules of the liquid. The distance between the molecules of liquid stays invariable. Due to the smallness of distance  *between them, we may assume that the vectors of speeds*  $v'_1$ ,  $v'_2$  of these molecules are applied to one point and lie in the same plane *xoy*. Then vector (9) also lies in this plane. Fig. 1 shows the position of vectors  $v'_1$ ,  $v'_2$ ,  $r'$ .

In the Supplement (see (6)) is shown that the magnitude of vector (9) is given by formula

$$
\Delta f = r \sin(\varphi_2 - \varphi_1). \tag{8}
$$

Taking into account (9, 10) we shall get:

$$
\Delta F = \sigma \sin(\varphi_2 - \varphi_1). \tag{9}
$$

This force appears when the adjacent molecules hit the barrier under different angles. We may assume that the summary force is applied to one of the molecules. Thus it creates a torque of dipole consisting of two molecules,

$$
M = r \cdot \Delta F. \tag{10}
$$

Each pair of adjacent molecules generates a dipole with a torque (10). The torques increase the local speeds of the liquid molecules, which, in its turn, increase the torques of the said dipoles. Because of this, the turbulence once began continues to grow, spreading in the liquid volume. Formula (9) determines the forces of gravito-magnetic interaction of the liquid molecules as a function of speeds of these contacting molecules.

These forces can be included to the Navier-Stokes equations as mass forces – see further.

#### **6. Example: Turbulent Water Flow in a Pipe**

Now we shall consider the case of interaction between liquid streams, assuming that the interaction is between groups of molecules forming an element of a stream. We shall take a specific case when the

**7**

speed vectors of the streams are the same  $|v_1| = |v_2| = v$  and also the masses of these groups are  $m_1 = m_2 = m$ . From (4) we can find

$$
\sigma = \zeta \xi G \left(\frac{mv}{cr}\right)^2.
$$
\n(11)

where r is the distance between the streams. Let us denote as d a typical size of the group (the stream diameter) and rewrite (11) as

$$
\sigma = \varsigma \xi G \left( \frac{\rho \cdot d^3 v}{cr} \right)^2.
$$
\n(11a)

where  $\rho$  is liquid density, and the mass of the group is

$$
m = \rho \cdot d^3. \tag{11B}
$$



Fig. 2 (from Vikipedia). Water vapor (1) and water (2). Molecules of water are enlarged by  $5.10^7$  times.

The further example is related to water. As in liquids the molecules are located at a distance commensurable with the size of molecule itself (see Fig. 2), we shall take the distance between molecules equal to the molecule diameter, w2which for water is  $r \approx 3 \cdot 10^{-12}$  [cm]. The water density is  $\rho = 1/g/cm^3$ . Let us find also the speed of water flow where the turbulence occurs. It is known [3], that the condition of turbulence occurrence is given by Reinolds criterion, which for a round pipe is  $Re = Dv / \eta$ , (12)

where  $D$  is the pipe's diameter,  $\eta$  is the kinematic viscosity coefficient - for water it is  $\eta \approx 0.01 \text{cm}^2/\text{sec}$  [5]. Let  $D = 2.5 \text{cm}$ ]. The turbulence occurs when the Reinolds number is  $\text{Re} > 2300$ . Now from (12) let us find the speed of turbulent flow:  $v = 10$  [cm/sec] Let the diameter of interacting streams  $d \approx 0.1$   $cm$ ]. It was mentioned above that  $\zeta = 2$ ,  $\xi \approx 10^{12}$ ,  $G \approx 7 \cdot 10^{-8}$ . Then from (11a) we find  $\sigma = 2 \cdot 10^{12} \cdot 7 \cdot 10^{-8} \left( 1 \cdot 0.1^3 \cdot 10 \cdot \left( 3 \cdot 10^{10} \cdot 3 \cdot 10^{-12} \right) \right)^2 \approx 2000 \, [\text{dynes}] \tag{13}$ Let us assume now that  $\sin(\varphi_2 - \varphi_1) \approx 10^{-2}$ . Then we shall find the force (9):

$$
\Delta F \approx 20 \,\text{[dynes]}.\tag{14}
$$

From (10, 14) we find torque:

$$
M \approx r \cdot \Delta F \approx 2 \text{ [dynes*cm]}.
$$
 (15)

#### **7. The Equations of Turbulent Flow**

Let us return to formula (5.1):

$$
\overline{F_{21}} = \frac{\varsigma \xi Gm^2}{c^2 r^3} \left( \overline{v_1} \times (\overline{v_2} \times \overline{r}) \right) \left[ dynes = \frac{g \cdot cm}{sec^2} \right].
$$
 (1)

Similarly to p. 5 we find

$$
\overline{\Delta F} = \mathcal{G} \cdot \overline{\Delta f} \,, \tag{2}
$$

where

$$
\mathcal{G} = \frac{\varsigma \xi G m^2}{c^2 r^3} \left[ \frac{g}{cm^2} \right],\tag{3}
$$

$$
\overline{\Delta f} = \mathcal{G}((\overline{v_1} \times (\overline{v_2} \times \overline{r})) - (\overline{v_2} \times (\overline{v_1} \times \overline{r})))
$$
\n(4)

Taking into account (11b), we rewrite (3) as

$$
\mathcal{G} = \frac{\varsigma \xi G \rho^2 d^6}{c^2 r^3} \left[ \frac{g}{cm^2} \right].
$$
\n(4a)

Further we shall denote the forces causing the turbulence, as Т. In the Supplement is shown (see also Fig. 1), that if all forces lie in one plane, then (4) is equivalent to formula

$$
T_y = \mathcal{G} \cdot R_x (v_{2x} v_{1y} - v_{2y} v_{1x}),
$$
\n(5)

where

 $T_{y}$  - is a force acting on the mass moving with speed  $v_{2},$ 

 $R<sub>x</sub>$  - the distance between the masses centers.

Let the two adjacent molecule groups are located on the *ох* axis*.* We denote

$$
R_x = dx,\tag{6a}
$$

$$
v_2 = v, \quad v_1 = v + dv. \tag{6B}
$$

Then

$$
T_y = \mathcal{G} \cdot dx \big( v_x \big( v_y + dv_y \big) - v_y \big( v_x + dv_x \big) \big) \tag{7}
$$

or

$$
T_y = \mathcal{G} \cdot dx \big( v_x dv_y - v_y dv_x \big). \tag{8}
$$

Similarly, for a right coordinate system we have:

$$
T_z = \mathcal{G} \cdot dy \Big( v_y dv_z - v_z dv_y \Big), \tag{9}
$$

$$
T_x = \mathcal{G} \cdot dz \left( v_z dv_x - v_x dv_z \right).
$$
\n<sup>(10)</sup>

Let us consider an operator (further for shortness sake we shall call it turbulean)

$$
R_x
$$
 - the distance between the masses centers.  
\nthe two adjacent molecule groups are located on the *ox* axis. We  
\n $R_x = dx$ , (6a)  
\n $V_2 = v$ ,  $v_1 = v + dv$ . (6b)  
\n $T_y = \theta \cdot dx (v_x (v_y + dv_y) - v_y (v_x + dv_x))$  (7)  
\n $T_y = \theta \cdot dx (v_x dv_y - v_y dv_x)$ . (8)  
\n $I_x = \theta \cdot dx (v_x dv_y - v_x dv_y)$ , (9)  
\n $T_x = \theta \cdot dz (v_z dv_x - v_x dv_z)$ . (10)  
\nus consider an operator (further for shortness sake we shall call i  
\n
$$
v_x \frac{dv_x}{dz} - v_x \frac{dv_z}{dz}
$$
\n
$$
\Omega(v) = \begin{vmatrix} v_z \frac{dv_x}{dz} - v_x \frac{dv_z}{dz} \\ v_y \frac{dv_y}{dy} - v_y \frac{dv_x}{dx} \end{vmatrix} \begin{bmatrix} cu \\ ce\kappa^2 \end{bmatrix}
$$
 (11)  
\nExample 1. We shall consider an ideal laminar flow in which  
\n $v_x \neq 0$ ,  $v_y = 0$ ,  $v_z = 0$ . Apparently here  $\Omega(v) = 0$ , i.e. lamina-  
\nallow cannot spontaneously become a turbulent flow.  
\n $R = dx = dy = dz$  (12)  
\n $n$  (10-12) follows the expression  
\n $T = R^2 g \cdot \Omega(v) \begin{bmatrix} cm^2 & \frac{g}{sec^2} & \frac{cm}{sec^2} = \frac{g \cdot cm}{sec^2} = \frac{d \cdot m}{sec^2} \end{bmatrix}$ . (13)  
\n $T = \Theta_1 \cdot \Omega(v) \text{[dynes]},$  (14)

**Example 1.** We shall consider an ideal laminar flow in which  $v_x \neq 0$ ,  $v_y = 0$ ,  $v_z = 0$ . Apparently here  $\Omega(v) = 0$ , i.e. laminar flow cannot spontaneously become a turbulent flow.

According to (6a) we have  
\n
$$
R = dx = dy = dz
$$
 (12)

From (10-12) follows the expression

$$
T = R^2 \mathcal{G} \cdot \Omega(v) \left[ cm^2 \frac{\text{g}}{cm^2} \cdot \frac{\text{cm}}{\text{sec}^2} = \frac{\text{g} \cdot \text{cm}}{\text{sec}^2} = \text{dynes} \right]. \tag{13}
$$

или

$$
T = \mathcal{G}_1 \cdot \Omega(v)[\text{dynes}],\tag{14}
$$

где

$$
\mathcal{G}_1 = R^2 \mathcal{G} = \frac{R^2 \zeta \xi G \rho^2 d^6}{c^2 r^3} [g].
$$
 (15)

The expression (14) defines a force acting on the group of molecules from the side of three adjacent molecule groups, located before the first group on the coordinate axes, if the differentials of the coordinates are equal to the distance between molecules (12). This force

is acting on the volume of four molecule groups, i.e. on volume  $4d^3$ . So the force acting on a unit volume is

$$
T_m = \rho_m \Omega(v) \left[ \frac{\text{dynes}}{\text{sm}^3} = \frac{\text{g}}{\text{sec}^2 \text{sm}^2} \right],\tag{16}
$$

where

$$
\rho_m = \frac{9}{4d^3} = \frac{R^2 \varsigma \xi G \rho^2 d^3}{4c^2 r^3} \left[ \frac{g}{cm^3} \right]
$$

or

$$
\rho_m = \frac{\varsigma \xi G \rho^2 d^8}{4c^2 r^3} \left[ \frac{\mathrm{g}}{\mathrm{cm}^3} \right],\tag{17}
$$

поскольку  $R \approx d$  .

**1 1** *g* Note for comparison, that in hydrodynamics equations, the dimension of mass force is I  $\rfloor$ 1  $\mathsf{I}$ L  $\frac{\text{dynes}}{\text{g}} = \frac{\text{cm}}{\text{sec}^2}$ cm g dynes *ec*  $F_m$   $\frac{F_{m}}{F_{m}} = \frac{F_{m}}{2}$ , and the dimension of force acting on a unit volume. I  $\rfloor$ 1  $\mathsf{I}$ L  $\frac{dynes}{g} = \frac{g}{sm^3} = \frac{dynes}{sm^3} = \frac{g}{sec^2cm^2}$ g s dynes s g g dynes *m m ec m*  $\mathcal{P}F_m$   $\frac{F_{m}}{2} = \frac{F_{m}}{2} = \frac{F_{m}}{2} = \frac{F_{m}}{2}$ . The dimension of force (16) is exactly the same. The coefficient (17) has the dimension of

density and it can be called the turbulent density of a liquid.

**Example 2.** Let us find the turbulent density  $\rho_m$  of water. We have:  $\rho = 1 \Big[ g/cm^3 \Big], d \approx 0.1 \Big[ cm \Big], c \approx 3.10^{10} \Big[ cm/sec \Big], \zeta = 2$ ,  $\xi \approx 10^{12}$ . Let the diameter of the stream is  $d \approx 0.1$  cm and the distance between the streams is  $r\approx\!10^{-8}$  [c*m*]. Then

$$
\rho_m = \frac{\varsigma \xi G \rho^2 d^8}{4c^2 r^3} = \frac{2 \cdot 10^{12} \cdot 7 \cdot 10^{-8} \cdot 10^{-8}}{4 \cdot (3 \cdot 10^{10})^2 (10^{-8})^3}
$$
  
or  $\rho_m \approx 0.4 \left[ \frac{\Gamma}{\text{cm}^3} \right].$ 

The forces (16) may be included into Navier-Stokes equations. The Navier-Stokes equations complemented by such forces become the equations of hydrodynamics for turbulent flow.

The turbulean (11) by its structure is similar to the expression

$$
(v \cdot \nabla)v = \begin{bmatrix} v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} + v_z \frac{\partial v_x}{\partial z} \\ v_x \frac{\partial v_y}{\partial x} + v_y \frac{\partial v_y}{\partial y} + v_z \frac{\partial v_y}{\partial z} \\ v_x \frac{\partial v_z}{\partial x} + v_y \frac{\partial v_z}{\partial y} + v_z \frac{\partial v_z}{\partial z} \end{bmatrix},
$$
(18)

appearing in the Navier-Stokes equation. Thus for turbulent flows calculations one may use the known method for the Navier-Stokes equations solution, including the method presented in [6, 7].

The expression (18) arrears in Navier-Stokes solution with a factor  $\rho$ . Consequently, the turbulean (11) can influence the equation's solution if the coefficient (17) will be equal  $\rho_m \approx \rho$ .

#### **Supplement**

Let us consider an expression with vectors

$$
\overline{f} = (\overline{a} \times (\overline{b} \times \overline{r})). \tag{1}
$$

In a right Cartesian coordinate system this expression will look as follows:

$$
\overline{f} = \begin{bmatrix} a_y(b_xr_y - b_yr_x) - a_z(b_zr_x - b_xr_z) \\ a_z(b_yr_z - b_zr_y) - a_x(b_xr_y - b_yr_x) \\ a_x(b_zr_x - b_xr_z) - a_y(b_yr_z - b_zr_y) \end{bmatrix}.
$$
\n(2)

Let us assume that the projections of these vectors on the *z* axis are equal to zero. Then

$$
\overline{f} = (b_x r_y - b_y r_x) \begin{bmatrix} a_y \\ -a_x \\ 0 \end{bmatrix}.
$$
 (2a)

Let us also assume that  $r_y = 0$ , i.e.  $r = r_x$ . Then

$$
\overline{f} = (b_x r_y - b_y r_x) - a_x
$$
\n
$$
\begin{bmatrix}\n\overline{f} = b_y \begin{bmatrix}\n\overline{f} = b_y \end{bmatrix}\n\begin{bmatrix}\n\overline{f} = b_y \end{bmatrix}\n\begin{bmatrix}\n\overline{f} = b_z \end{bmatrix}
$$
\n
$$
\begin{bmatrix}\n\overline{f} = b_z \end{bmatrix}\n\begin{bmatrix}\n\overline{f} = b_z \end{bmatrix}\n\begin{bmatrix}\n\overline{f} = b_z \end{bmatrix}\n\begin{bmatrix}\n\overline{f} = b_z \end{bmatrix}\n\begin{bmatrix}\n\overline{f} = b_z \end{bmatrix}
$$
\n
$$
\begin{bmatrix}\n\overline{f} = b_z \end{bmatrix}\n\begin{bmatrix}\n\overline{f} = b_z \end{bmatrix}\n\begin{bmatrix}\n\overline
$$

So, in the assumed conditions

$$
\overline{f}_{ab} = (\overline{a} \times (\overline{b} \times \overline{r})) = rb_y \begin{vmatrix} -a_y \\ a_x \end{vmatrix}.
$$
 (3a)

Similarly

$$
\overline{f}_{ba} = (\overline{b} \times (\overline{a} \times (-\overline{r}))) = -ra_y \begin{vmatrix} -b_y \\ b_x \end{vmatrix}.
$$

We have

$$
\overline{\Delta f} = \overline{f}_{ab} + \overline{f}_{ba} = r \left( \begin{array}{c} 0 \\ a_x b_y - a_y b_x \end{array} \right) \tag{4}
$$

or

$$
\overline{\Delta f_y} = r(a_x b_y - a_y b_x) = rab(\cos\varphi_a \sin\varphi_b - \sin\varphi_a \cos\varphi_a), \quad (5)
$$

where  $\varphi_a$ ,  $\varphi_b$  - the angles of vectors a, b with the axis  $\mathcal{O}x$ . Thus, vector  $\Delta f$  lies in the same plane where the initial vectors are located, this vector is directed along *оу* axis and has the value

$$
\Delta f = rab \sin(\varphi_b - \varphi_a). \tag{6}
$$

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